NASA TECHNICAL MEMORANDUM

NASA TM X-64534

INTERPOLATION OF BODE'S TABLES OF THE SOLAR CONTINUOUS ABSORPTION COEFFICIENT

By Edward M. Wadsworth Space Sciences Laboratory

July 1, 1970

CASE FILE COPY

NASA

George C. Marshall Space Flight Center Marshall Space Flight Center, Alabama

| | | | | IDARD TITLE PAGE |
|--|---|---|---------------------------------------|---------------------|
| 1. REPORT NO. TM X-64534 | 2. GOVERNMENT ACCES | SSION NO. | 3. RECIPIENT'S | CATALOG NO. |
| 4. TITLE AND SUBTITLE | | | 5. REPORT DATE | |
| Interpolation of Bode's Tables of | f the Solar Continuo | us Absorption | July 1, 1 | 970 |
| Coefficient | | | | DRGANIZATION CODE |
| 7. AUTHOR(S) Edward M. Wadsworth | | WEAT | 8. PERFORMING OF | GANIZATION REPORT # |
| 9. PERFORMING ORGANIZATION NAME AND A | ADDRESS | | 10. WORK UNIT, NO |), |
| George C. Marshall Space Fligh | t Center | | | |
| Marshall Space Flight Center, A | labama 35812 | | 11. CONTRACT OR | GRANT NO. |
| | | | 13. TYPE OF REPO | RT & PERIOD COVERED |
| 12. SPONSORING AGENCY NAME AND ADDRES | 5S | | · · · · · · · · · · · · · · · · · · · | |
| | | | Téchnical M | emorandum |
| | | | 14. SPONSORING | AGENCY CODE |
| 15. SUPPLEMENTARY NOTES | A second | | | |
| Prepared by Space Sciences Lab | oratory, Science ar | d Engineering D | irectorate | |
| 16. ABSTRACT | | | | |
| Knowledge of the total co | ntinuous absorption | coefficient for a | wide range of | f wavelengths |
| is vital to many areas of solar p | hysics, such as the | construction of | model atmospl | heres and line |
| profile calculations. Recently, | • | | | |
| absorption coefficient for the sur | - | | | |
| temperatures. To obtain the abs | | | | |
| temperature at an untabulated wa | | | | |
| the several wavelengths listed, | | | | |
| | | | | |
| wavelength. At a given waveleng | | | | |
| pressures not given in the table | • | | | |
| paper describes a computer subp | - | | o calculate the | e solar |
| continuous absorption coefficient | t for any given mode | el atmosphere. | | |
| | | | | |
| | | | | |
| | | | | |
| | | | | |
| | | | | |
| | | | | |
| | | | | |
| | | | | |
| | | | | |
| | | | | |
| 17. KEY WORDS | 18 | . DISTRIBUTION STAT | TEMENT | |
| | | For Public Re | lease | |
| | | | , | |
| | | Mona 1 | - Idna | 100.0 |
| | 4 | , , ora | , full | , wid |
| 19. SECURITY CLASSIF, (of this report) | 20. SECURITY CLASSIF | (of this page) | 21. NO. OF PAGES | 22. PRICE |
| Unclassified | Unclassified | · (· · · · · · · · · · · · · · · · · · | 16 | \$3.00 |

ACKNOWLEDGMENT

The assistance of Dr. Mona Hagyard of the Space Sciences Laboratory is gratefully acknowledged.

HO BUT THE HARBY AND

TABLE OF CONTENTS

| | and the state of t | _ |
|-------|--|-----|
| SUMMA | ARY | |
| INTRO | DUCTION | 1 |
| THE T | ECHNIQUE OF DOUBLE INTERPOLATION | 2 |
| CONCI | LUSIONS | 6 |
| APPEN | IDIX A: COMPUTER FLOW CHART | 8 |
| APPEN | NDIX B: COMPUTER SUBPROGRAM | 9 |
| REFER | RENCES | 10 |
| | | |
| | LIST OF TABLES | |
| Table | Title | age |
| 1. | Values of Log (Pe/K) | 2 |
| 2A. | Constant Log (Pe) Values; Log (Pe) = -2.5 | 3. |
| 2B. | Constant Log (Pe) Values; Log (Pe) = -2.0 | 3 |
| 3A. | Constant θ Values; $\theta = 1.25$ | 4 |
| 3B. | Constant θ Values; $\theta = 1, 20, \ldots$ | 4 |

TECHNICAL MEMORANDUM X-64534

INTERPOLATION OF BODE'S TABLES OF THE SOLAR CONTINUOUS ABSORPTION COEFFICIENT

SUMMARY

Knowledge of the total continuous absorption coefficient for a wide range of wavelengths is vital to many areas of solar physics, such as the construction of model atmospheres and line profile calculations. Recently, Gerhard Bode [1] compiled a set of tables for the continuous absorption coefficient for the sun covering a wide range of wavelengths, electron pressures, and temperatures. To obtain the absorption coefficient as a function of electron pressure and temperature at an untabulated wavelength, one can employ standard interpolation formulas using the several wavelengths listed, which are between major absorption edges and span the desired wavelength. At a given wavelength the absorption coefficients at particular temperatures and pressures not given in the table can be obtained by a double linear interpolation scheme. This paper describes a computer subprogram which has been developed to calculate the solar continuous absorption coefficient for any given model atmosphere.

INTRODUCTION

The subprogram used to interpolate the Bode data employs a method of two-way differences. This method is described in detail by Scarborough [2].

It is hoped that an example problem of the technique of two-way differences will clarify the procedure used to interpolate the Bode tables by computer. A flow chart (Appendix A) is also used to indicate the processes undertaken by the computer; the subroutine is listed in Appendix B.

THE TECHNIQUE OF DOUBLE INTERPOLATION

The example problem uses a table of values of log (electron pressure/absorption coefficient) at 5250.20 Å vs log (electron pressure) and θ , where θ is 5040/absolute temperature.

It should be noted that there is no Bode table for 5250. 20 Å; rather Table 1 was compiled using a simple straight-line interpolation of a Bode table at 4500.00 Å and one at 5698. 50 Å.

| | Log (Pe) | | | | | |
|----------|--------------|---------|---------------|---------|---------|---------|
| θ | -2. 5 | -2.0 | -1. ,5 | -1.0 | -0, 5 | 0.0 |
| 1. 30 | 24, 376 | 24. 569 | 24, 658 | 24, 693 | 24,713 | 24, 758 |
| 1. 25 | 24. 412 | 24, 625 | 24.727 | 24, 767 | 24. 784 | 24.806 |
| 1, 20 | 24. 443 | 24.681 | 24, 797 | 24. 884 | 24, 861 | 24.872 |
| 1, 15 | 24. 465 | 24.729 | 24, 865 | 24. 922 | 24.942 | 24.950 |
| 1.10 | 24. 452 | 24.767 | 24, 927 | 24. 999 | 25.024 | 24.033 |
| 1.05 | 24. 313 | 24, 768 | 24. 985 | 25.072 | 25. 105 | 25.117 |
| 1.00 | 23. 914 | 24. 627 | 25.004 | 25, 138 | 25. 183 | 25. 202 |
| 0, 95 | 23. 298 | 24. 200 | 24, 879 | 25. 174 | 25. 255 | 25. 281 |

TABLE 1. VALUES OF LOG (Pe/K)

Suppose that a value of log (Pe/K) is needed for particular values of θ and log (Pe) not given in Table 1. The method of two-way differences would then be used as follows:

Problem: Log (Pe/K) needs to be calculated at a θ value of 1.22 and a log (Pe) value of -2.2 at 5250.20 A.

Solution: Tables 2A and 2B show forward differences for constant log (Pe) values, and Tables 3A and 3B show differences for constant θ values (hence, two-way differences). A general formula for double interpolation uses these differences in providing the desired value of log (Pe/K). Note that log (Pe/K) = 24.412 at θ = 1.25 and log (Pe) = -2.5 is used as a "starting point" for taking differences. The starting point is that value of

 \log (Pe/K) in Table 1 for which the corresponding values of \log (Pe) and θ are closest to and above those which are being interpolated.

TABLE 2A. CONSTANT LOG (Pe) VALUES; LOG (Pe) = -2.5

| | 77 (0 0 5) | $\Delta^{1+0} \stackrel{\mathbf{a}}{\kappa}_{\theta 0}$ | $\Delta^{2+0} \overset{\mathbf{a}}{\kappa}_{\theta 0}$ |
|-------------------|------------|--|--|
| $\theta_0 = 1.25$ | 24. 412 | 0.031 | |
| $\theta_1 = 1.20$ | 24. 443 | 0. 022 | -0.009 |
| $\theta_2 = 1.15$ | 24. 465 | | |

TABLE 2B, CONSTANT LOG (Pe) VALUES; LOG (Pe) = -2.0

| | K(θ, -2.0) | $\Delta^{1+0}^{a}_{\kappa_{\theta 1}}$ | $\Delta^{2+0}^{\mathbf{a}}_{\kappa_{\theta 1}}$ |
|-------------------|------------|--|---|
| $\theta_0 = 1.25$ | 24, 625 | 0,074 | |
| $\theta_1 = 1.20$ | 24, 699 | 0,030 | -0.044 |
| $\theta_2 = 1.15$ | 24, 729 | | |

a. K₀₀ is the starting point for taking differences;

$$K(\theta, Log Pe) = Log (Pe/K)$$

$$\Delta^{1+0} \kappa_{\theta \text{ Pe}}$$

$$\Delta^{0+1} \kappa_{\theta \text{ Pe}}$$
= First-order difference,

$$\left. \begin{array}{l} \Delta^{2+0} \kappa \\ \Delta \\ \Delta^{0+2} \kappa \\ \theta \operatorname{Pe} \end{array} \right\} = \operatorname{Second-order\ difference.}$$

Also,

$$\Delta^{1+1}\kappa_{\theta Pe} = \Delta^{1+0}\kappa_{\theta 1} - \Delta^{1+0}\kappa_{\theta 0} = \Delta^{0+1}\kappa_{1Pe} - \Delta^{0+1}\kappa_{0Pe}$$

TABLE 3A. CONSTANT θ VALUES; $\theta = 1.25$

| TITLE WIS CONDITION OF THE PROPERTY OF THE PRO | | | | |
|--|-----------------|-----------------------------|-----------------------------------|--|
| | K(1.25, Log Pe) | $\Delta^{0+1}^{a}_{\kappa}$ | $\Delta^{0+2}^{a}_{\kappa_{1Pe}}$ | |
| $Log Pe_0 = -2.5$ | 24, 412 | 0,213 | | |
| $\log \text{ Pe}_{1} = -2.0$ | 24. 625 | 0.102 | -0.111 | |
| Log Pe ₂ = -1.5 | 24, 727 | 0.102 | | |

TABLE 3B. CONSTANT θ VALUES; $\theta = 1.20$

| | K(1, 20, Pe) | $\Delta^{0+1}^{a}_{\kappa}$ 1Pe | $\Delta^{0+2}^{a}_{\kappa}$ 1Pe |
|-------------------|--------------|---------------------------------|---------------------------------|
| Log $Pe_0 = -2.5$ | 24, 443 | 0, 256 | |
| $Log Pe_1 = -2.0$ | 24. 699 | 0.098 | -0.158 |
| $Log Pe_2 = -1.5$ | 24. 797 | 0.000 | |

a. K_{00} is the starting point for taking differences;

$$K(\theta, Log Pe) = Log (Pe/K)$$

$$\left. \begin{array}{c} \Delta^{2+0} \kappa_{\theta \, \mathrm{Pe}} \\ \Delta^{0+2} \kappa_{\theta \, \mathrm{Pe}} \end{array} \right\} = \text{Second-order difference.}$$

Also,

$$\Delta^{1+1}\kappa_{\theta\,\mathrm{Pe}} = \Delta^{1+0}\kappa_{\theta\,\mathbf{1}} - \Delta^{1+0}\kappa_{\theta\,\mathbf{0}} = \Delta^{0+1}\kappa_{1\mathrm{Pe}} - \Delta^{0+1}\kappa_{0\mathrm{Pe}}$$

The general formula for double interpolation using two-way differences is:

$$\begin{split} \mathbf{K} &= \mathbf{K}_{00} + \mathbf{u} \cdot \Delta^{1+0} \kappa_{00} + \mathbf{v} \cdot \Delta^{0+1} \kappa_{00} + \frac{1}{2!} \left[\mathbf{u} (\mathbf{u} - 1) \cdot \Delta^{2+0} \kappa_{00} \right. \\ &+ 2 \mathbf{u} \cdot \mathbf{v} \cdot \Delta^{1+1} \kappa_{00} + \mathbf{v} (\mathbf{v} - 1) \cdot \Delta^{0+2} \kappa_{00} \right] \end{split}$$

 \cdot where

$$u = \frac{\theta - \theta_0}{\theta_1 - \theta_0}$$

and

$$v = \frac{\text{Log (Pe)} - \text{Log (Pe)}_0}{\text{Log (Pe)}_1 - \text{Log (Pe)}_0}$$

From Table 1,

$$K_{00} = 24.412$$

$$\Delta^{1+0} \kappa_{00} = 0.031$$

$$\Delta^{0+1} \kappa_{00} = 0.213$$

$$\Delta^{2+0} \kappa_{00} = -0.009$$

$$\Delta^{0+2} \kappa_{00} = -0.111$$

Also,

$$\Delta^{1+1} \kappa_{00} = \Delta^{1+0} \kappa_{\theta 1} - \Delta^{1+0} \kappa_{\theta 0} = 0.043$$

For u and v:

$$v = \frac{-2.3 - (-2.5)}{0.5} = 0.4$$

Then,

$$Log (Pe/K) = 24.412 + (0.6) (0.031) + (0.4) (0.213)$$

$$+ \frac{1}{2} \left[(0.6) (-0.4) (-0.009) + 2(0.6) (0.4) (0.043) + (0.4) (-0.06) (-0.111) \right] = 24.541$$

Before the computer takes differences from Table 1, it first finds a suitable starting point. In the preceding example the computer would go to 24.412 to start taking differences. If a θ value of 1.12 and a log (Pe) value of -1.1 were read into the computer, the calculations would begin at 24.865 as a starting point. The computer scans those values of θ and log (Pe) in Table 1 until it finds the ones that are closest to but higher in the table than the θ and log (Pe) values read in. Then the log (Pe/K) value corresponding to these values of θ and log (Pe) is used as a starting point for taking differences. In this way the best possible interpolated value of log (Pe/K) is obtained.

CONCLUSIONS

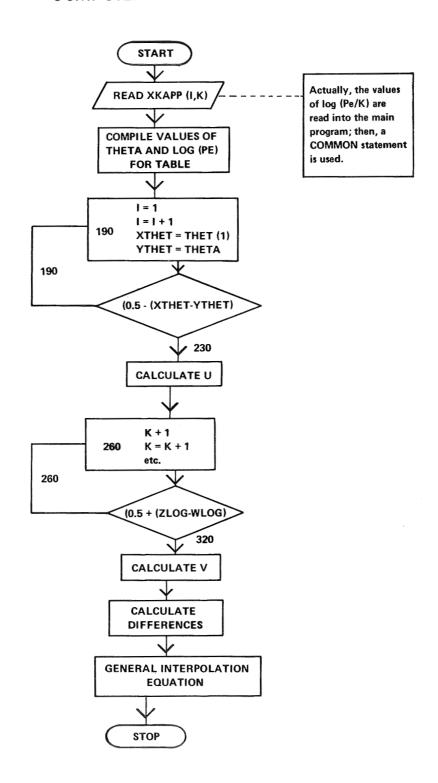
Some restrictions on using the subroutine should be mentioned. In Table 1, the values of θ must increase by equal amounts (-0.05 in this case); similarly, the values of log (Pe) must increase by equal steps.

For the subroutine to function, it must be able to take first- and second-order differences from Table 1. As long as the value of θ in the

interpolation is not equal to or smaller than 1.00 and the value of log (Pe) is not equal to or greater than -0.05, the calculations in the subroutine will be carried out. If this restriction is not observed, the table must be made larger, or the interpolation subroutine must be made to take only first-order differences.

APPENDIX A

COMPUTER FLOW CHART



COMPUTER SUBPROGRAM

&FOR, IS OPAC SUBROUTINE OPAC(X,THETA,PE,WV,AKCG) DIMENSION XKAPP(9,7), XLOG(7), THET(9) COMMON XKAPP THE!(1)=1.35 90 DO 100 I=2.9 100 THET(I)=THET(I=1)=.05 CONTINUE XLOG(1)=-3.0 120 DO 130 K=2.7 130 XLOG(K)=XLOG(K-1)+.5 CONTINUE 160 XTHET=0.0 170 YTHET=0.0 180 I = 1190 [=[+] 200 XTHET=THET(I) YTHET=THETA 220 IF (.05-(XTHET-YTHET)) 190,230,230 230 U=0.0 240 U=(XTHET=YTHET)/=05 250 K = 1260 K=K+1 -270 ZLOG=0.0 280 -ZLOG=XLOG(K) 290 WLOG=0.0 WLOG= •434294*ALOG(PE) 310 IF (.5+(ZLOG-WLOG)) 260,320,320 320 V=0.0 330 V=(WLOG-ZLOG)/.5 340 FIRT=0.0 350 FIRT=XKAPP(I+1,K)-XKAPP(I,K) 360 SECT=0.0 370 SECT=XKAPP(I+2,K)-XKAPP(I+1,K) 380 --FIRL=0.40-390 FIRL=XKAPP(I,K+1)-XKAPP(I,K) 400 SECL=0.0 410 SECL=XKAPP(I,K+2)=XKAPP(I,K+1) 420 SECTO=0.0 430 SECTO=SECT-FIRT 440 SECLO=0.0 450 SECLO=SECL-FIRL 460 DA=0.0 470 DA=XKAPP(I+1,K+1)-XKAPP(I,K+1) 480 DX=0.0 490 DX=DA-FIRT 500 XCAP=0.0 510 1.)*V)/2. XAKCG=0.0 XAKCG=23.6203-(XCAP-WLOG) Y=0.0 Y=XAKCG*2.30258 AKCG=0.0 AKCG=EXP(Y) RETURN END

REFERENCES

- 1. Bode, Gerhard: Die kontinuierliche Absorption von Sternatmosphären in Abhängigkeit von Druck, Temperatur und Elementhäufigkeiten. Institut für Theoretische Physik und Sternwarte der Universität Kiel, Germany, 1965.
- 2. Scarborough, James B.: Numerical Mathematical Analysis. The Johns Hopkins Press, Baltimore, Md., 1950.

APPROVAL

INTERPOLATION OF BODE'S TABLES OF THE SOLAR CONTINUOUS ABSORPTION COEFFICIENT

By Edward M. Wadsworth

The information in this report has been reviewed for security classification. Review of any information concerning Department of Defense or Atomic Energy Commission programs has been made by the MSFC Security Classification Officer. This report, in its entirety, has been determined to be unclassified.

This document has also been reviewed and approved for technical accuracy.

WILLIAM C. SNODDY

Chief, Space Thermophysics Division

GERHARD B. HELLER

Director, Space Sciences Laboratory

DISTRIBUTION

INTERNAL

S&E-SSL-DIR

Mr. Gerhard B. Heller Mr. Ray V. Hembree

S&E-SSL-C

Reserve (10)

S&E-SSL-N

Dr. Rudolf Decher Mr. Henry Stern

S&E-SSL-P

Dr. Robert Naumann

S&E-SSL-S

Dr. Werner Sieber

S&E-SSL-T

Mr. William Snoddy

S&E-SSL-TE

Mr. Edgar Miller

S&E-SSL-TR

Mr. Gary Arnett

S&E-SSL-TT

Mr. Billy P. Jones

Dr. Mona Hagyard (5)

Dr. Allen Gary

Mr. Daniel Gates

Mr. Ted Calvert

Mr. Creighton Miller

Mr. Paul Craven

Mr. James Watkins

Mr. Edward Wadsworth (10)

A&TS-MS-IP (2)

A&TS-MA-PT

Mr. Mark Russell

A&TS-MS-IL (8)

A&TS-TU (6)

A&TS-MS-H

PM-PR-M

A&TS-PAT

L. D. Wofford, Jr.

DEP-T

DIR

EXTERNAL

Scientific and Technical Information

Facility (25)

P. O. Box 33

College Park, Maryland 20740

Attn: NASA Representative (S-AK/RKT)